

Volume 11, Issue 4, PP 79-89, ISSN: 2360-9194, March, 2021 Double Blind Peer Reviewed International Research Journal garcjournalssubmit@gmail.com Journal Series: Global Academic Research Consortium (garc)

# Effect of High Temperature on Mechanical Properties of Concrete Containing Platicizers and Retarding Water Reducing Admixtures

#### Babagana Kachalla

Department of Civil Engineering, Mai Idris Alooma Polytechnic Geidam, Yobe State. Corresponding Email address: Bgkachalla@miapoly.edu.ng

**Abstract**: The properties of concrete exposed to high temperature conditions are considerably influenced by the cooling regime. Therefore, the study investigated the effect of high temperature on mechanical properties of concrete containing admixtures. Mix design was in accordance to ASTM C-494 Type B with uniform water/binder (w/b) ratio of 0.5 and mix ratio of 1:2:4 was adopted. Furthermore, the additives used was mls/100kg of cement. Specimens were cured for 7, 14, 21 and 28 days at room temperature. At the end of the curing periods, the specimens were left to dry in the air for (2 hrs) prior to heating. The concrete specimens heated to different levels of controlled high temperatures after curing; the average compressive strengths under the 6 different elevated temperatures for 7, 14, 21, and 28days age concretes were found to be 35.89 N/mm<sup>2</sup>, 39.71 N/mm<sup>2</sup>, 44.03 N/mm<sup>2</sup> and 46.01 N/mm<sup>2</sup> respectively. Therefore, higher compressive strength was recorded in 28 days' age concrete containing Super Plasticizer. However, the average compressive strengths under the 6 different elevated temperatures for 7, 14, 21, and 28 days' age concretes were found to be 33.18 N/mm<sup>2</sup>, 36.80 N/mm<sup>2</sup>, 40.20 N/mm<sup>2</sup> and 42.15 N/mm<sup>2</sup> respectively. Therefore, higher compressive strength was recorded in 28 days' age concrete containing plasticizer. The average compressive strengths under the 6 different elevated temperatures for 7, 14, 21, and 28 days' age concretes were found to be 34.52 N/mm<sup>2</sup>, 38.97 N/mm<sup>2</sup>, 41.42 N/mm<sup>2</sup> and 41.77 N/mm<sup>2</sup> respectively. Therefore, higher compressive strength was recorded in 28 days' age concrete containing retarding and water reducing agent.

Keywords: Additives, Particle Size, Concrete, Temperature and Strength

#### Introduction

Concrete is a composite construction material, composed of cement (commonly Portland cement) and other cementitious materials such as fly ash and slag cement, aggregate (generally a coarse aggregate made of gravels or crushed rocks such as limestone, or granite, plus a fine aggregate such as sand), water, and admixtures. Material scientists, chemists, engineers, and manufacturers' technical representatives have helped the concrete industry to improve ability to control work times, workability, strength, and durability of Portland cement concrete by adding some supplementary substances named

admixtures. The function of each admixture focuses on aa specific need, and each has been developed independently of the others. Some admixtures already have chemistry that affects more than one property of concrete, and some have simply been combined for ease of addition during the batching process.

The properties of concrete exposed to high temperature conditions are considerably influenced by the cooling regime. The specimens were either dry cooled (in air) or wet cooled (quenched) in water (Xiao, 2004; Kowalski 2008; Husem 2006). Rapid cooling (quenching) was found to have a much more deteriorating effect on the mechanical properties of concrete as compared to dry cooling (Xiao, 2004; Husem, 2006). The differences are particularly pronounced at lower

#### **Sponsored by TETFund**

temperatures to become hardly noticeable at the test temperature of 600 °C (Xiao, 2004). Similarly, the influence of cooling method (dry or wet) on the mechanical properties of concrete becomes insignificant when the time of quenching is shortened to about 10 sec.

The different tests to determine the high temperature performance of concrete use different specimens in terms of shape and size (Behnood & Ghandehari 2009; Noumowe 2005; Drzymała & Bednarek 2011a) with cylindrical specimens expected to enhance obtaining uniform temperature distribution throughout the specimen. However, cubes and rectangular prisms of various sizes are also used in such tests (Poon et al. 2001; Arioz 2007; Ergün et al. 2013). It has been demonstrated that the specimen size has no effect on the properties of concrete exposed to high temperature simulating fire conditions.

According to EN 1992-1-2:2008/NA:2010P (2010) the tensile strength of concrete exposed to elevated temperature decreases linearly from 100 °C up to 600 °C at which it has no tensile strength at all. Actually, while it is true that exposure to elevated temperature affects the tensile strength of concrete, this decrease is not as big as to lead to zero tensile strength at 600 °C (Neville 2012; Xiao, 2004; Saad et al. 1996).While according to Neville (2012) the decrease of tensile strength of concrete exposed to elevated temperature follows a similar pattern to the decrease of compressive strength. Many researchers found it to be much greater as compared to the decrease in compressive strength, resulting in a considerable increase in brittleness of concrete (Xiao, König 2004; Chen et al. 2009). Exposure to elevated temperature affects also the flexural strength of concrete. The increase in temperature results in a decrease in flexural strength (Husem 2006; Pliya et al. 2011; Ergün et al. 2013). According to Bazant and Kaplan, (1996) results, which indicated that for a wide variety of ordinary concrete mixes made with conventional aggregates, there was a reduction in strength after heating to 500°C from a minimum 15% to a maximum 60%. Results also indicated that there is an approximately linear reduction in the strength ratios as the temperature increases from 200°C to 500°C. The result at higher temperatures indicated that at 600°C, the residual compressive strength ratios vary between about 80 and 25%. At 700°C, the ratios vary between 70 and 20%. At 800°C, the ratios vary between 50 and 20% of the initial unheated compressive strength.

#### Methodology

#### **Concrete Mix Design**

Mix design was in according to ASTM C-494 Type B with uniform water/binder (w/b) ratios of 0.5 and mixes ratio of 1:2:4 was adopted. Furthermore, curing ages of 7, 14, 21 and 28 days were used. The additives used was based on amount recommended by the manufacturer and as shown in Tble 1.

Table	1:	Admixtures	Dosage
rubic		i uniment co	Dobuge

Concrete Mix	Concrete Mix	Concrete Mix	Concrete Mix
Design	Design	Design	Design
	(Rheobuild 800)	(Pozzolith 322N)	(Retarding and
			Water Reducing
			Agent 100Ri)
Dosage (mls/100kg of cement)	1000	327.5	195

#### Table 2: Experimental Specimens

Types of Specimen	Super plasticizer		Retarding and	Control
	(Rheobuild 800)	(Pozzolith	Water Reducing	
		322N)	(Pozzolith100Ri)	
No. of Cubes	3x4	3x4	3x4	1x4x3
Total required cubes		48X6		

A total of two hundred and eighty-eight (288) concrete cubes of different Admixtures and elevated temperatures of 100,150,200,300,400 and 600 °c were used. Thirteen (6) run experiments, 3 replications and 4 different curing ages (7, 14, 21 and 28days) which makes a total of 288 cubes. Figure 1 shows cube cast and curing.



Figure 1: Cubes cast and Curing

#### Concrete Heating and Cooling Process

The concrete specimens heated to different levels of high temperatures after curing; using an electrical furnace with a maximum temperature of (1000 °C). The electric furnace was consisted of wide chamber of a double metal containing auto-control thermal probes; with

built in thermocouples. The temperature of the furnace increases by an average value of  $(5^{\circ}C/min)$  at its primary stage up to  $(200^{\circ} C)$ , becoming faster to about  $(10^{\circ} C/min)$  at the required temperature. The concrete specimens then placed inside the furnace for one hour at a constant temperature; then specimens were left for (24 hrs) to be air cooled.

#### Results and Discussion Grain size distributions from sieve analysis

able 5.1 life 5a			JIII SIEVE allaly	313	
Diameter (mm)	Mass of Sieve (g)	Mass of Sieve & Soil (g)	Soil Retained (g)	Soil Retained (%)	Soil Passing (%)
2.36	468.00	491	23.0	5.3	94.7
1.00	506.00	534	28.0	6.5	88.2
0.60	498.00	564	66.0	15.3	72.9
0.40	447.00	513	66.0	15.3	57.5
0.30	323.00	351	28.0	6.5	51.0
0.21	352.00	401	49.0	11.4	39.7
0.15	443.00	487	44.0	10.2	29.5
0.080	502.000	598	96.0	22.3	28.8
Pan	490	521	31.0	7.2	32.5
		TOTAL:	431.0	100.0	

Table 3: Fine Sand Grain size distributions from sieve analysis

#### Fine Modules = 3.6

ASTM D422-63(2007) classified fine aggregates range from a Fineness Modulus (FM) 2.00 to 4.00. Therefore, the soil classified as fine aggregate.

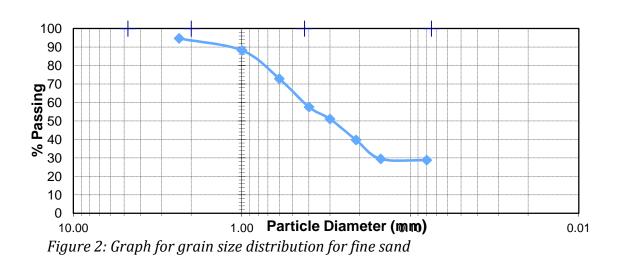


Table 4: Compressive Strength of Concrete containing Super Plasticized Under Elevated Temperature

Temperature (°C)	Identification of Specimen	Weight before placing in electric Oven (Kg)	Weight after placing in electric Oven (Kg)	(after heating)	(Kg/m <sup>3</sup> )	Average compressive strength (KN/mm²): 7 days Age	Average compressive strength (KN/mm²) 14 davs age	Average compressive strength (KN/mm²): 21 days age	Average compressive strength (KN/mm²): 28 days age	Average compressive strength (KN/mm <sup>2</sup> ) (Control)
100	1JU 1 1JU 2 1JU 3	8.54 8.56 8.45	8.52 8.53 8.54	2524 2527 2530	2527	20.56	23.04	25.07	26.67	26.59
150	1JU 11 1JU 12 1JU 13	8.55 8.53 8.56	8.46 8.52 8.51	2507 2524 2521	2517	20.08	23.64	25.67	26.17	26.01
200	1JU 21 1JU 22 1JU 23	8.56 8.55 8.57	8.42 8.45 8.44	2495 2504 2501	2500	19.78	22.33	24.79	25.01	22.52
300	1JU 31 1JU 32 1JU 33	8.58 8.56 8.54	8.39 8.38 8.37	2486 2483 2480	2483	18.22	19.24	21.56	22.56	23.24
400	1JU 41 1JU 42 1JU 43	8.57 8.55 8.58	8.26 8.14 8.28	2447 2412 2453	2437	15.60	16.33	18.82	19.34	18.19
60 0	1JU 51 1JU 52 1JU 53	8.56 8.54 8.57	8.16 8.17 8.14	2418 2421 2412	2417	13.44	14.56	16.18	18.27	15.45

Table 5: Compressive Strength of Concrete containing Plasticized under Elevated Temperature

Temperature (°C)	Identification of Specimen	Weight before placing in electric Oven (Kg)	ter Ove	Density of cupe (kg/m²) (after heating)	(Kg/m <sup>3</sup> )	Average compressive strength (KN/mm²) 7 days age	Average compressive strength (KN/mm²)14 days age	Average compressive strength (KN/mm²) 21 days age	Average compressive strength (KN/mm²) 28 days age	Average compressive strength (KN/mm <sup>2</sup> ) (Control)
	2JU 1 2JU	8.58	8.58	2542						
100	2 2JU 3	8.57 8.58	8.56 8.57	2536 2539	2539	20.05	22.41	23.87	24.22	24.85
	2JU J	8.59	8.51	2521						
150	2JU 12	8.58	8.52	2524	2522	20.01	21.82	23.51	24.35	24.67
	2JU 13	8.57	8.51	2521						

	2JU 21	8.59	8.43	2498						
200	2JU 22	8.58	8.46	2507	2505	18.91	20.33	22.41	23.02	23.42
	2JU 23	8.59	8.47	2510						
	2JU 31	8.57	8.42	2495						
300	2JU 32	8.59	8.39	2486	2487	17.11	19.43	20.45	22.12	22.76
	2JU 33	8.58	8.37	2480						
	2JU 41	8.57	8.29	2478						
400	2JU 42	8.58	8.18	2587	2526	13.34	15.24	17.01	18.11	19.36
	2JU 43	8.58	8.34	2512						
	2JU 51	8.58	8.17	2406						
600	2JU 52	8.57	8.16	2457	2436	10.12	11.18	13.34	14.62	15.14
	2JU 53	8.57	8.14	2445						

#### Table 6: Compressive Strength of Concrete Containing Retarding and Water Reducing Agent Under Elevated Temperature

	g		ß			Sz	ys	ys	ys	(lo
	Identification of Specimen	Weight before placing in electric Oven (Kg)	Weight after placing in electric Oven (Kg)	Density of cube (Kg/m³) (after heating)	- 410	Average compressive strength (KN/mm²) 7 days age	Average compressive strength (KN/mm²) 14 days age	Average compressive strength (KN/mm²) 21 days age	Average compressive strength (KN/mm²) 28 days age	Average compressive strength (KN/mm²) (Control)
	Spec	ight before placin; electric Oven (Kg)	ter Ove	Density or cupe /m³) (after heat		Average compressive ength (KN/mm²) 7 da age	Average compressive ength (KN/mm²) 14 d age	Average compressive ength (KN/mm²) 21 di age	Average compressive ength (KN/mm²) 28 di age	Average compressive ngth (KN/mm²) (Cont
G	of	re p ver	Weight after in electric Ov	or d ter	(Kg/m <sup>3</sup> )	comp N/mn age	comp J/mm age	comp J/mm age	comp J/mm age	um <sup>2</sup>
)₀) ə	tion	efo) ic C	eigh elec	sity I (af	Kg/	e co KN, aξ	e co ξN/	e co KN/ aξ	e co KN/ aξ	e co N/r
ture	ficat	ht b ectr	We in e	m <sup>3</sup> )	ر ا	rag th (	rag h (F	rag h (F	rag h (F	rag 1 (K
era	entil	eig] ele	ing	L Kg/		Ave eng	Ave	Ave	Ave	Ave ngtŀ
Temperature (∘C)	Ide	N	plac			str	stre	stre	stre	treı
Τe										s
100	3JU 1 3JU 2	8.52	8.50	2519	2522	20.05	22.02	22.00	04 70	
100	3JU 3	8.52 8.55	8.51 8.54	2521 2530	2523	20.35	22.92	23.98	24.72	25.85
	2111 1 1 2111	8.53								
150	3JU 11 3JU 12		8.51 8.53	2521 2527	2524	20.15	22.80	23.67	24.44	25.52
150	3JU 13	8.54 8.53	8.52	2527	2524	20.15	22.00	23.07	24.44	25.52
	3JU 21 3JU	8.52	8.50	2519						
200	22	8.54	8.53	2527	2525	19.81	21.43	22.72	23.37	24.36
	3JU 23	8.57	8.54	2530						
	3JU 31 3JU	8.56	8.49	2516						
300	32	8.52	8.48	2513	2515	18.75	20.84	21.41	21.02	23.12
	3JU 33	8.53	8.49	2516						
	3JU 41 3JU	8.57	8.26	2447						
400	42	8.55	8.14	2412	2437	14.25	16.65	18.12	17.83	20.68
	3JU 43	8.58	8.28	2453						
	3JU 51 3JU	8.56	8.16	2418						
60	52	8.54	8.17	2421	2417	10.25	12.28	14.35	13.92	15.25
0	3JU 53	8.57	8.14	2412						

donerete containing	Super rius	CICIZCI				
Source of Variation	SS	df	MS	F	P-value	F critical
Between Groups	245.05	11	22.28	2.75	0.048	2.72
Within Groups	97.35	12	8.11			
_						
Total	342.40	23				
Alpha value = 0.05						
Alpha value > P – val	lue					

Table 7: ANOVA Analysis for compressive strength variation between the curing ages of Concrete containing Super Plasticizer

Therefore, compressive strength between the concrete of 7, 14, 21 and 28 days are not the same. However, the average compressive strengths under the 6 different elevated temperatures for 7, 14, 21, and 28 days age concretes were found to be 35.89 N/mm<sup>2</sup>, 39.71 N/mm<sup>2</sup>, 44.03 N/mm<sup>2</sup> and 46.01 N/mm<sup>2</sup> respectively. Therefore, higher compressive strength is recorded in 28 days age Concrete containing Super Plasticizer.

Table 8: ANOVA Analysis for compressive strength variation between the curing ages of Concrete containing Plasticizer

Source of Variation	SS	df	MS	F	P-value	F critical
Between Groups	256.04	11.00	23.28	6.05	0.019	4.03
Within Groups	23.07	6.00	3.85			
Total	279.11	17.00				
Alpha value = 0.05						
Alpha value > P – val	ue					

The difference is significant

The difference is significant

Therefore, compressive strength between the concrete of 7, 14, 21 and 28 days are not the same. However, the average compressive strengths under the 6 different elevated temperatures for 7, 14, 21, and 28 days age concretes were found to be 33.18 N/mm<sup>2</sup>, 36.80 N/mm<sup>2</sup>, 40.20 N/mm<sup>2</sup> and 42.15 N/mm<sup>2</sup> respectively. Therefore, higher compressive strength is recorded in 28 days age Concrete containing Plasticizer.

Table 9: ANOVA Analysis for compressive strength variation between the curing ages of Concrete containing Retarding and Water Reducing Agent

Source of						
Variation	SS	df	MS	F	P-value	F critical
Between Groups	333.10	11	30.28	6.88	0.0011	2.71
Within Groups	52.77	12	4.39			
-						
Total	385.88	23				
Alpha value = 0.05						
Alpha value > P – v	value					

#### The difference is significant

Therefore, compressive strength between the concrete of 7, 14, 21 and 28 days are not the same. However, the average compressive strengths under the 6 different elevated temperatures for 7, 14, 21, and 28 days age concretes were found to be 34.52 N/mm<sup>2</sup>, 38.97 N/mm<sup>2</sup>, 41.42 N/mm<sup>2</sup> and 41.77 N/mm<sup>2</sup> respectively. Therefore, higher compressive strength is recorded in 28 days age Concrete containing Retarding and Water Reducing Agent.

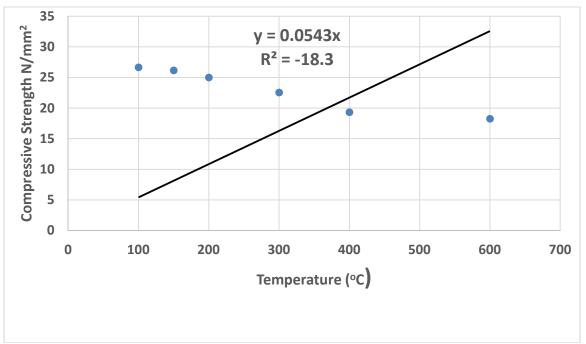


Figure 3: Compressive Strength of Concrete containing Super Plasticized Under Elevated Temperature

Figure 3 is regression graph showing inverse relationship between temperature and compressive strength of concrete containing Super Plasticizer with a  $R^2$  value of -ve 18.3. Meaning, the higher the temperature the lower the compressive strength as shown in the figure.

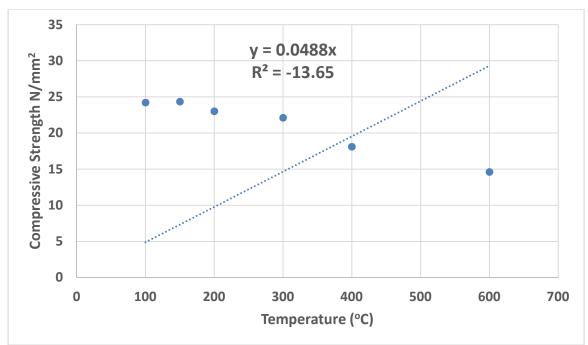


Figure 4: Compressive Strength of Concrete containing Plasticized Under Elevated Temperature

Figure 4 is regression graph showing inverse relationship between temperature and compressive strength of concrete containing Plasticizer with a R<sup>2</sup> value of -ve 13.65. Meaning, the higher the temperature the lower the compressive strength as shown in the figure.

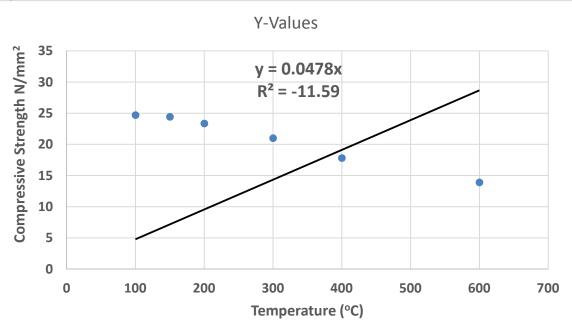


Figure 5: Compressive Strength of Concrete containing Water Reducing Agent Under Elevated Temperature

Figure 5 is regression graph showing inverse relationship between temperature and compressive strength of concrete containing Retarding and Water Reducing Agent with a

 ${
m R}^2$  value of -ve 11.59. Meaning, the higher the temperature the lower the compressive strength as shown in the figure.

Table 10: ANOVA analysis on effects of Super Plasticizer, Plasticizer, Retarding and Water
Reducing Agent on Concrete compressive strength

Source of						
Variation	SS	df	MS	F	P-value	F critical
Between Groups	903.48	11	82.13	18.37	2.52E-15	1.95
Within Groups	268.29	60	4.47			
Total	1171.77	71				
Alpha value = 0.05						
Alpha value > P – value						

The difference is significant

Therefore, effect of the three additives used are not the same on compressive strength of concrete containing Super Plasticizer, Plasticizer, Retarding and Water Reducing Agent. However, highest average value of 46.01N/mm<sup>2</sup> was observed at 28 days age concrete containing Plasticizer.

#### Conclusion

The study determined the compressive strength of concrete containing superplasticizer, plasticizer and retarding water reducing admixtures at varying Temperature. Therefore, the following conclusions were drawn:

- i. The compressive strength between the concrete of 7, 14, 21 and 28 days are not the same. However, the average compressive strengths under the 6 different elevated temperatures for 7, 14, 21, and 28 days age concretes were found to be 35.89 N/mm2, 39.71 N/mm2, 44.03 N/mm2 and 46.01 N/mm2 respectively. Therefore, higher compressive strength is recorded in 28 days' age Concrete containing Super Plasticizer.
- The compressive strength between the concrete of 7, 14, 21 and 28 days are not the same. However, the average compressive strengths under the 6 different elevated temperatures for 7, 14, 21, and 28 days' age concretes were found to be 33.18 N/mm2, 36.80 N/mm2, 40.20 N/mm2 and 42.15 N/mm2 respectively. Therefore, higher compressive strength is recorded in 28 days' age Concrete Containing Plasticizer.
- iii. The compressive strength between the concrete of 7, 14, 21 and 28 days are not the same. However, the average compressive strengths under the 6 different elevated temperatures for 7, 14, 21, and 28 days' age concretes were found to be 34.52 N/mm2, 38.97 N/mm2, 41.42 N/mm2 and 41.77 N/mm2 respectively. Therefore, higher compressive strength is recorded in 28 days' age Concrete Containing Retarding and Water Reducing Agent.
- iv. Therefore, effect of temperature on the three additives used are not the same on compressive strength of concrete containing Super Plasticizer, Plasticizer, Retarding

and Water Reducing Agent. However, highest average value of 46.01N/mm2 was observed at 28 days' age concrete containing Super Plasticizer.

#### References

- Arioz, O. (2007). Effects of elevated temperatures on properties of concrete, Fire Safety Journal 42(8): 516–522. <u>https://doi.org/10.1016/j.firesaf.2007.01.003</u>
- Bazant Z.P. and Kaplan, M.F. (1996) "Concrete at high temperature; Material properties and mathematical models", Longman Group Ltd, London.
- Behnood, A.; Ghandehari, M. (2009). Comparison of compressive and splitting tensile strength of high-strength concrete with and without polypropylene fibers heated to high temperatures, Fire Safety Journal 44(8): 1015–1022. https://doi.org/10.1016/j.firesaf.2009.07.001
- Drzymała, T.; Bednarek, Z. 2011a. Analysis of the values of modulus of elasticity measured after exposure to elevated temperature of high-performance concrete reinforced with polypropylene fibres, Logistyka 6 (in Polish).
- EN 1992-1-2:2008/NA: 2010P, Eurocode 2: Design of concrete structures. Parts 1-2: General rules. Structural fire design. Eu-ropean Standards Committee, 2010.
- Ergün, A.; Kürklü, G.; Başpınar, M. S.; Mansour, M. Y. 2013. The effect of cement dosage on mechanical properties of concrete exposed to high temperatures, Fire Safety Journal 55: 160–167.
- Husem, M. 2006. The effects of high temperature on compressive and flexural strengths of ordinary and high-performance concrete, Fire Safety Journal 41(2): 155–163. https://doi.org/10.1016/j.firesaf.2005.12.002
- Kowalski, R. 2008. Computational evaluation of reinforced concrete components loaded in bending under fire conditions. Warsaw: Warsaw Polytechnic Publishing House (in Polish).
- Neville, A. M. 2012. Properties of concrete. Cracow: Polski Cement.
- Noumowe, A. (2005). Mechanical properties and microstructure of high strength concrete containing polypropylene fibres exposed to temperatures up to 200 °C, Cement and Concrete Research 35(11): 2192–2198.
- Poon, C.-S.; Azhar, S.; Anson, M.; Wong, Y.-L. 2001. Comparison of the strength and durability performance of normal- and high-strength pozzolanic concretes at elevated temperatures, Cement and Concrete Research 31(9): 1291–1300. https://doi.org/10.1016/S0008-8846(01)00580-4
- Xiao, J.; König, G. 2004. Study on concrete at high temperature in China an overview, Fire Safety Journal 39(1): 89–103. <u>https://doi.org/10.1016/S0379-7112(03)00093-6</u>